

ECE 171A: Linear Control System Theory

Lecture 9: Review

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Announcements

- ▶ HW2 due by tonight
- ▶ Midterm exam (I) — in class, April 22 (Friday in Week 4)
 - **Scope:** Lectures 1 - 10, HW1 - HW3, DI 1-4; (Reading materials in the textbook)
 - Closed book, closed notes, closed external links.
 - **Come on time** (1 or 2 minutes early if you can; we will start at 9:00 am promptly)
 - No MATLAB is required. No graphing calculators are permitted. A basic arithmetic calculator is allowed.
 - The exams must be done in a blue book. Bring a blue book with you.
 - **No collaboration and discussions are allowed.** It is dishonest to cheat on exams. Instances of academic dishonesty will be referred to the Office of Student Conduct for adjudication. *You don't want to take a risk for such a small thing.*

Outline

Review: Lectures 1 - 8

Two Exercises

Outline

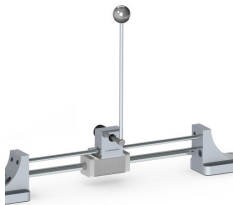
Review: Lectures 1 - 8

Two Exercises

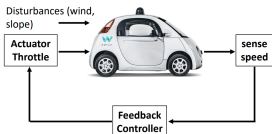
Lecture 1 - Overview of control systems

A **control system** is an interconnection of two or more dynamical systems that provides a **desired response**.

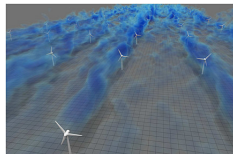
- ▶ Control is to modify the inputs to the plant to produce a **desired output**.



(a) Inverted Pendulum



(b) Cruise control



(c) Wind farm

- ▶ Feedforward control vs. feedback control
- ▶ Two live experiments
- ▶ **Feedback control = Sensing + Computation + Actuation**

Lecture 2 - ODEs and the first control example

Review on ODEs

- ▶ An n th-order linear ordinary differential equation (ODE) is:

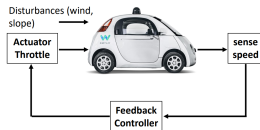
$$\frac{d^n}{dt^n}y(t) + a_{n-1}\frac{d^{n-1}}{dt^{n-1}}y(t) + \dots + a_1\frac{d}{dt}y(t) + a_0y(t) = u(t)$$

- ▶ First-order matrix ODE

$$\dot{x} = Ax(t) + Bu(t)$$

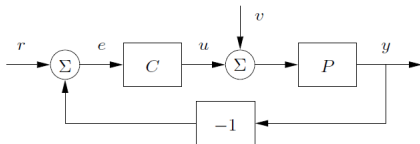
Cruise control

P control $F_{\text{engine}} = K_p e(t)$
I control $F_{\text{engine}} = K_i \int_0^t e(t) dt$
D control $F_{\text{engine}} = K_d \frac{d}{dt} e(t)$



Feedback control = Sensing + Computation + Actuation

Lecture 3 - Feedback principles



- ▶ We have considered static plant dynamics with analytical solutions

$$y = \text{sat}(x) = \begin{cases} -1 & \text{if } x \leq -1 \\ x & \text{if } |x| < 1 \\ 1 & \text{if } x \geq 1 \end{cases}$$

- ▶ and a simple dynamical model with numerical simulations
- ▶ to illustrate several fundamental properties of feedback

- ▶ Disturbance attenuation
- ▶ Reference signal tracking
- ▶ Robustness to uncertainty
- ▶ Shaping of dynamical behavior

Lecture 4/5 - System modeling

A model is a *mathematical representation* of a physical, biological, or information system.

- ▶ Models allow us to reason about a system and make predictions about how a system will behave.
- ▶ The model we choose depends on the questions we wish to answer, and so there may be multiple models for a single dynamical system.
- ▶ It is important to keep in mind that all models are an approximation of the underlying system.

The choice of state is not unique.

- ▶ There may be many choices of variables that can act as the state.
 - A trivial example: One can choose different units (scaling factors)
 - A less trivial example: One can take sums and differences of some variables.

Lecture 4/5 - System modeling

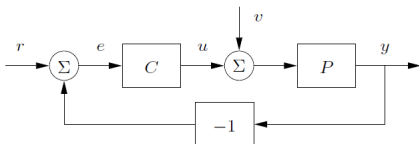
- ▶ $x \in \mathbb{R}^n$: state; $y \in \mathbb{R}^p$: output; $u \in \mathbb{R}^m$: input
- ▶ Continuous-time (e.g., speed control, inverted pendulum, spring-mass)

$$\begin{aligned} \dot{x} &= f(x, u) \\ y &= h(x, u) \end{aligned} \iff \begin{aligned} \dot{x} &= Ax + Bu \\ y &= Cx + Du. \end{aligned}$$

- ▶ Discrete-time (e.g., consensus protocol, predator-prey dynamics)

$$\begin{aligned} x[k+1] &= f(x[k], u[k]), \\ y[k] &= h(x[k], u[k]). \end{aligned} \iff \begin{aligned} x[k+1] &= Ax[k] + Bu[k], \\ y[k] &= Cx[k] + Du[k]. \end{aligned}$$

- ▶ **Block diagrams:** Emphasize the information flow and to hide details of the system.

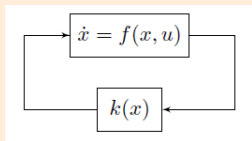


Lecture 6 - System solutions and Phase portraits

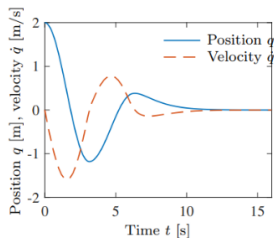
Closed-loop system: with $u = k(x)$

$$\dot{x}(t) = f(x, k(x)) := F(x).$$

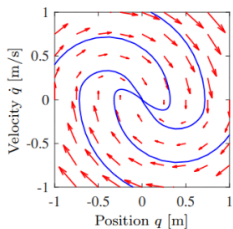
Analytical or *Computational* solutions



- ▶ Solving differential equations
- ▶ Qualitative analysis: phase portraits and time plot



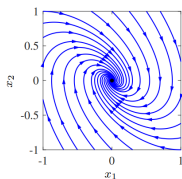
(a) Time plot



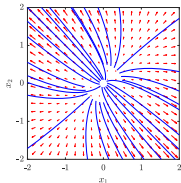
(b) Phase portrait

Lecture 7 - Equilibrium and stability

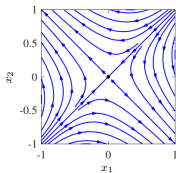
- ▶ An **equilibrium** point of a dynamical system represents a *stationary* condition for the dynamics.
- ▶ Stable, asymptotically stable, unstable; terminology like sink, source, saddle, center



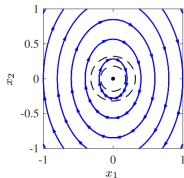
(a) Sink



(b) Source



(c) Saddle



(d) Center

- ▶ Stability of linear systems $\dot{x} = Ax$
 - Eigenvalue test
 - **Routh–Hurwitz** Criterion (will be reviewed again in week 5/6)

Lecture 8: Jacobian Linearization

Consider a nonlinear system $\dot{x} = F(x)$, with $x_e = 0$ as an equilibrium point. Let

$$A = \left. \frac{\partial F}{\partial x} \right|_{x_e=0}$$

- ▶ $x_e = 0$ is locally asymptotically stable if A is asymptotically stable or all eigenvalues of A have negative real parts.
- ▶ $x_e = 0$ is unstable if one or more of the eigenvalues of A has positive real part.

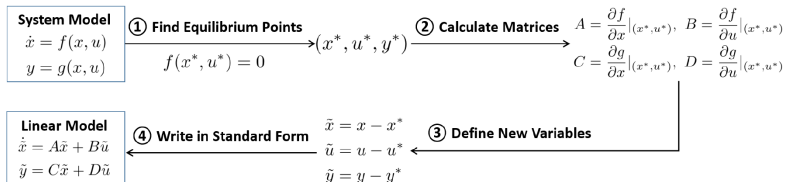


Figure: Model Linearization Procedure (Taken from Prof Na Li's ES 155)

Outline

Review: Lectures 1 - 8

Two Exercises

Exercise A: Linearization of nonlinear systems

Consider the following dynamical system

$$\begin{aligned}\dot{x}_1 &= x_1 - x_2^2 \\ \dot{x}_2 &= 2x_1 - x_2^2 - x_1x_2.\end{aligned}$$

1. Determine the equilibrium point(s) of this system
2. Linearize the system around the equilibrium point(s)
3. Are the equilibrium points stable for the linearized system?

Solution:

- Let $f_1(x_1, x_2) = 0, f_2(x_1, x_2) = 0$.

$$\begin{aligned}x_1 - x_2^2 &= 0 \\ 2x_1 - x_2^2 - x_1x_2 &= 0.\end{aligned} \Rightarrow \begin{cases} x_1^* = 0 \\ x_2^* = 0 \end{cases}, \begin{cases} x_1^* = 1 \\ x_2^* = 1 \end{cases}$$

- Define the dynamics

$$\begin{aligned}f_1(x_1, x_2) &= x_1 - x_2^2 \\ f_2(x_1, x_2) &= 2x_1 - x_2^2 - x_1x_2.\end{aligned}$$

Exercise A: Linearization of nonlinear systems

- ▶ Compute their partial derivatives

$$\begin{aligned}\frac{\partial f_1}{\partial x_1} &= 1, & \frac{\partial f_1}{\partial x_2} &= -2x_2, \\ \frac{\partial f_2}{\partial x_1} &= 2 - x_2, & \frac{\partial f_2}{\partial x_2} &= -2x_2 - x_1\end{aligned}$$

- ▶ For the first equilibrium $x_1^* = 0, x_2^* = 0$, there is no need to define new variables $\tilde{x}_1 = x_1 - x_1^* = x_1$. We have

$$\begin{aligned}\dot{x}_1 &= x_1 \\ \dot{x}_2 &= 2x_1.\end{aligned} \quad \Rightarrow \quad \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 2 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

- ▶ For the second equilibrium point $x_1^* = 1, x_2^* = 1$, we define $\tilde{x}_1 = x_1 - 1$, $\tilde{x}_2 = x_2 - 1$, and we have

$$\begin{aligned}\dot{\tilde{x}}_1 &= \tilde{x}_1 - 2\tilde{x}_2 \\ \dot{\tilde{x}}_2 &= \tilde{x}_1 - 3\tilde{x}_2.\end{aligned} \quad \Rightarrow \quad \begin{bmatrix} \dot{\tilde{x}}_1 \\ \dot{\tilde{x}}_2 \end{bmatrix} = \begin{bmatrix} 1 & -2 \\ 1 & -3 \end{bmatrix} \begin{bmatrix} \tilde{x}_1 \\ \tilde{x}_2 \end{bmatrix}$$

Exercise A: Linearization of nonlinear systems

- ▶ For the first linearized system

$$\det(\lambda I - A) = \det \left(\begin{bmatrix} \lambda - 1 & 0 \\ -2 & \lambda \end{bmatrix} \right) = (\lambda - 1)\lambda = 0$$
$$\Rightarrow \lambda_1 = 1, \lambda_2 = 0$$

This is unstable since $\lambda_1 = 1$ has positive real part.

- ▶ For the second linearized system

$$\det(\lambda I - A) = \det \left(\begin{bmatrix} \lambda - 1 & 2 \\ -1 & \lambda + 3 \end{bmatrix} \right) = \lambda^2 + 2\lambda - 1 = 0$$
$$\Rightarrow \lambda = -1 \pm \sqrt{2}$$

This is unstable since $\lambda_2 = -1 + \sqrt{2}$ has positive real part.

Exercise A: Linearization of nonlinear systems

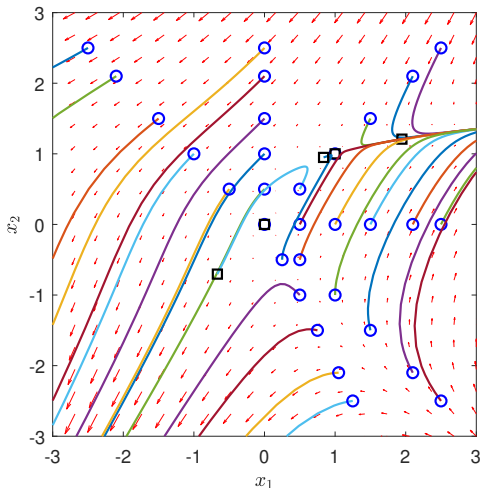


Figure: Phase portrait of the nonlinear system:

$$\dot{x}_1 = x_1 - x_2^2, \dot{x}_2 = 2x_1 - x_2^2 - x_1x_2.$$

Example B: SpaceX rocket controller design

A rocket of mass m in vertical flight can be modeled by

$$\begin{aligned}\dot{h} &= v \\ M\dot{v} &= F - \frac{km}{h^2} - cv,\end{aligned}$$

- ▶ $h > 0$ is the vertical distance away from the earth,
- ▶ v is the vertical velocity,
- ▶ F is the rocket engine thrust force (control input),
- ▶ $\frac{km}{h^2}$ represents the universal gravitation, and cv captures the friction.

Suppose $m = 1, k = 1, c = 1$; we let $x_1 = h$ and $x_2 = v$, and the output $y = h$, input $u = F$.

Question 1 - equilibrium point: Let $F^* = 1$. What is the equilibrium point of this system?

$$\begin{aligned}\dot{x}_1 &= x_2 \\ \dot{x}_2 &= -\frac{1}{x_1^2} - x_2 + u\end{aligned} \quad \Longrightarrow \quad \begin{cases} u^* = 1, x_1^* = 1, x_2^* = 0, \\ y^* = x_1^* = 1 \end{cases}$$

Example: SpaceX rocket controller design

Question 2 - Linearization: Linearize the system around the equilibrium point.

- ▶ **Step 1:** Write down the (possibly nonlinear) dynamics (step 0: obtain the equilibrium)

$$\begin{cases} \dot{x}_1 = f_1(x_1, x_2, u) = x_2 \\ \dot{x}_2 = f_2(x_1, x_2, u) = -\frac{1}{x_1^2} - x_2 + u \end{cases}$$

- ▶ **Step 2:** compute their partial derivatives

$$\begin{aligned} \frac{\partial f_1}{\partial x_1} &= 0, & \frac{\partial f_1}{\partial x_2} &= 1, & \frac{\partial f_1}{\partial u} &= 0, \\ \frac{\partial f_2}{\partial x_1} &= \frac{2}{x_1^3}, & \frac{\partial f_2}{\partial x_2} &= -1, & \frac{\partial f_2}{\partial u} &= 1, \end{aligned}$$

- ▶ **Step 3:** define new variables $\tilde{x} = x - x^*$, $\tilde{u} = u - u^*$, and $\tilde{y} = y - y^*$.
- ▶ **Step 4:** Finalize the linearized model

$$\begin{bmatrix} \dot{\tilde{x}}_1 \\ \dot{\tilde{x}}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 2 & -1 \end{bmatrix} \begin{bmatrix} \tilde{x}_1 \\ \tilde{x}_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} \tilde{u}, \quad \tilde{y} = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} \tilde{x}_1 \\ \tilde{x}_2 \end{bmatrix}.$$

Example: SpaceX rocket controller design

Question 3 - controller design: SpaceX hover (and landing) test¹ - design a controller to stabilize the rocket at the equilibrium point.

$$\tilde{u} = K_1 \tilde{x}_1 + K_2 \tilde{x}_2.$$

If $K_1 = -2.25$, $K_2 = 0.5$, is the linearized system stable?

► **Step 1:** write down the closed-loop system

$$\begin{aligned}\tilde{u} &= [K_1 \quad K_2] \begin{bmatrix} \tilde{x}_1 \\ \tilde{x}_2 \end{bmatrix} = [K_1 \quad K_2] \tilde{x} \\ \Rightarrow \begin{bmatrix} \dot{\tilde{x}}_1 \\ \dot{\tilde{x}}_2 \end{bmatrix} &= \begin{bmatrix} 0 & 1 \\ 2 & -1 \end{bmatrix} \begin{bmatrix} \tilde{x}_1 \\ \tilde{x}_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} [K_1 \quad K_2] \begin{bmatrix} \tilde{x}_1 \\ \tilde{x}_2 \end{bmatrix} \\ &= \begin{bmatrix} 0 & 1 \\ 2 + K_1 & -1 + K_2 \end{bmatrix} \begin{bmatrix} \tilde{x}_1 \\ \tilde{x}_2 \end{bmatrix}\end{aligned}$$

¹Videos: <https://youtu.be/07Pm8ZY0XJI>; <https://youtu.be/1sJlFzUQVmY>

Example: SpaceX rocket controller design

Question 3 - controller design: SpaceX hover (and landing) test² - design a controller to stabilize the rocket at the equilibrium point.

$$\tilde{u} = K_1 \tilde{x}_1 + K_2 \tilde{x}_2.$$

If $K_1 = -2.3125$, $K_2 = 0.5$, is the linearized system stable?

- ▶ **Step 1:** write down the closed-loop system

$$\dot{\tilde{x}} = \begin{bmatrix} 0 & 1 \\ 2 + K_1 & -1 + K_2 \end{bmatrix} \begin{bmatrix} \tilde{x}_1 \\ \tilde{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -0.3125 & -0.5 \end{bmatrix} \begin{bmatrix} \tilde{x}_1 \\ \tilde{x}_2 \end{bmatrix}$$

- ▶ **Step 2:** analyze the eigenvalues of the closed-loop system

$$\begin{aligned} \det(\lambda I - A) &= \det \left(\begin{bmatrix} \lambda & -1 \\ 0.3125 & \lambda + 0.5 \end{bmatrix} \right) = \lambda^2 + 0.5\lambda + 0.3125 \\ &= (\lambda + 0.25)^2 + 0.25 \end{aligned}$$

its eigenvalues are $\lambda = -0.25 \pm 0.5i$, which is stable.

²Videos: <https://youtu.be/07Pm8ZY0XJI>; <https://youtu.be/1sJ1FzUQVmY>