

Simulation results on Kalman filter, Paper B15

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Q4.

```
%% Q4
clc;clear; close all
m = 7700;

A = [0 -1/m; 0 0]; F = [0;1]; V = 1; W = 1; C = [1 0];

% X = are(A, B, C) returns the stabilizing solution (if it
% exists) to the continuous-time Riccati equation:
%      A'*X + X*A - X*B*X + C = 0

P = are(A',C'*W^(-1)*C,F*V*F')
Kf = P*C'*W^(-1)

v0 = 40;

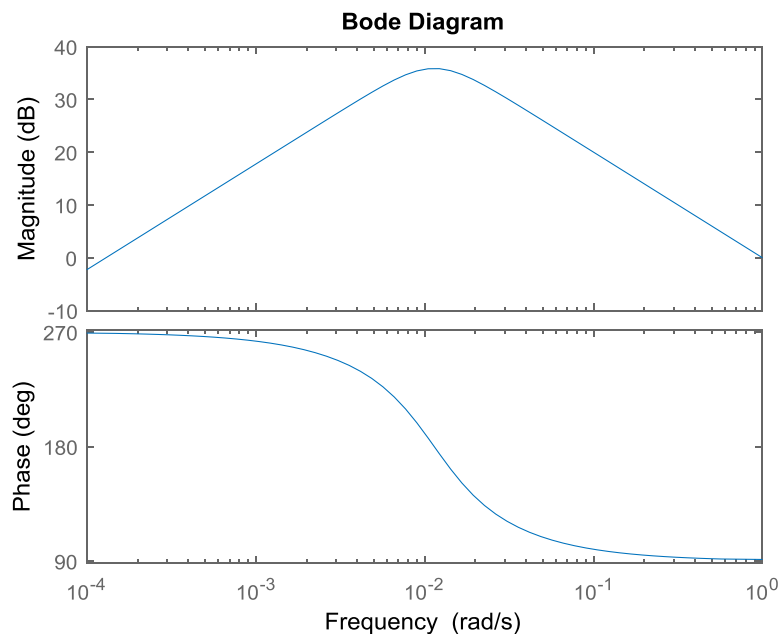
%% b)
A1 = [0 -1/m; 0 -0.6*v0^2/m];
P1 = are(A1',C'*W^(-1)*C,F*V*F')
Kf1 = P1*C'*W^(-1)
```

Filter frequency response:

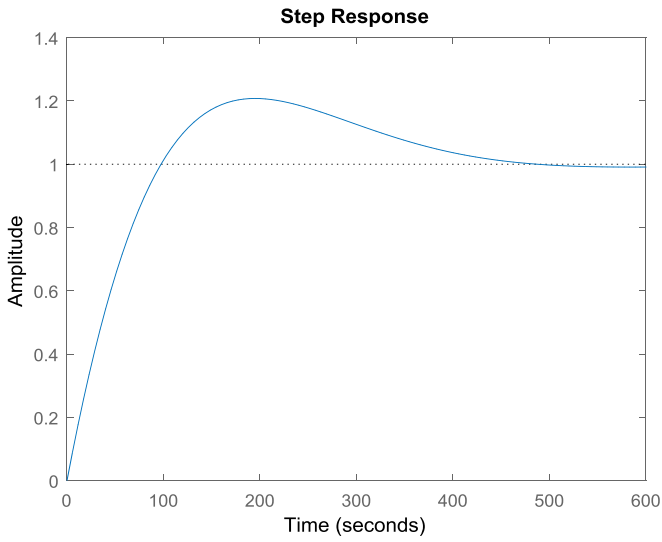
The first Kalman filter: constant aero-drag model

$$K_{f1} = \begin{bmatrix} 0.0161 \\ -1 \end{bmatrix}$$

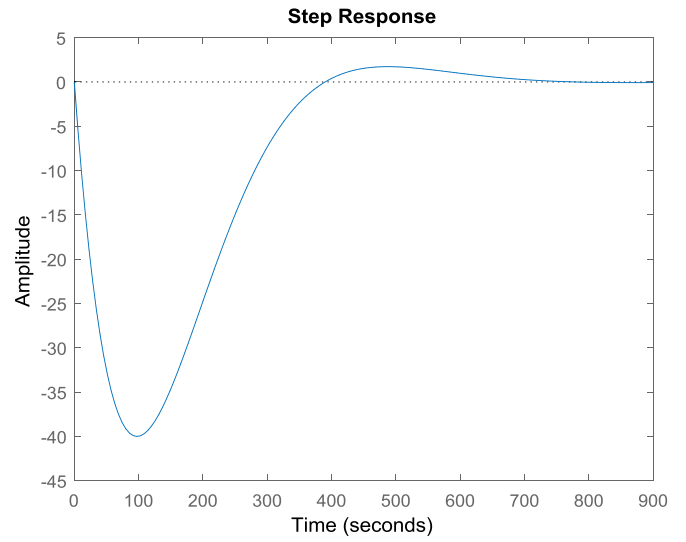
Transfer function from the velocity measurement y to the estimate of aero-drag D_a



Step response (unite change of velocity measurement; check the output of aero-drag)



(a) estimate of velocity

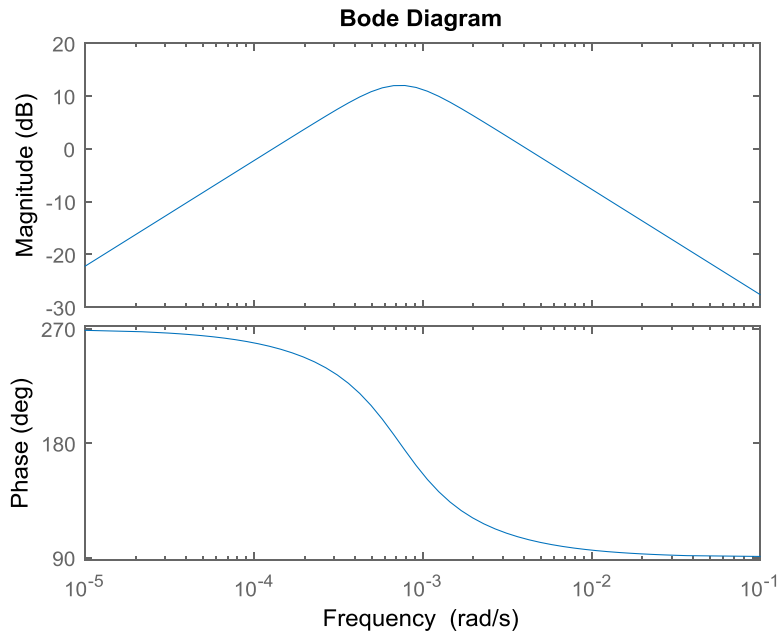


(b) estimate of aero-drag

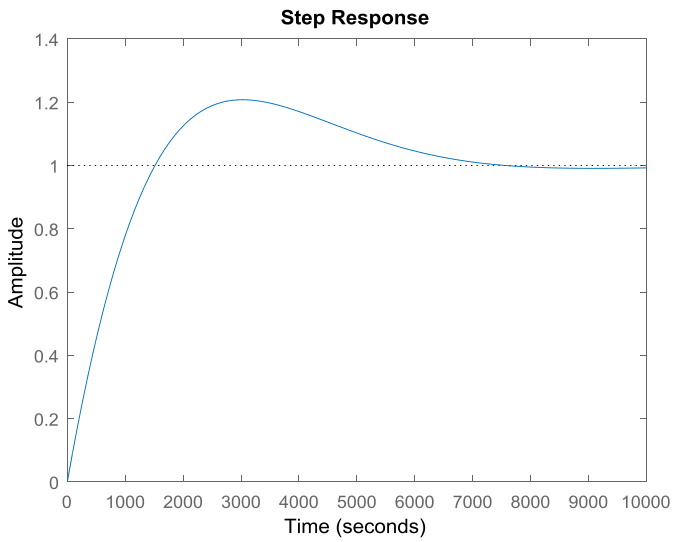
The second Kalman filter: non-constant aero-drag model

$$K_{f1} = \begin{bmatrix} 0.001 \\ -0.0041 \end{bmatrix}$$

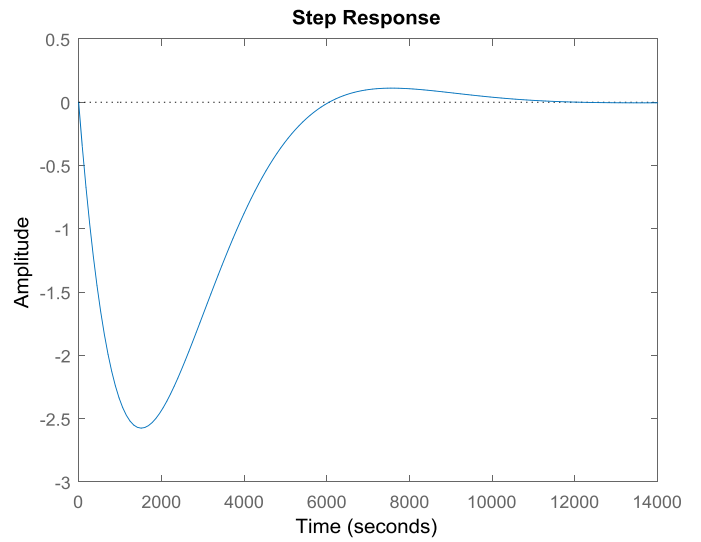
Transfer function from the velocity measurement y to the estimate of aero-drag D_a



Step response (unite change of velocity measurement; check the output of aero-drag)



(a) estimate of velocity



(b) estimate of aero-drag

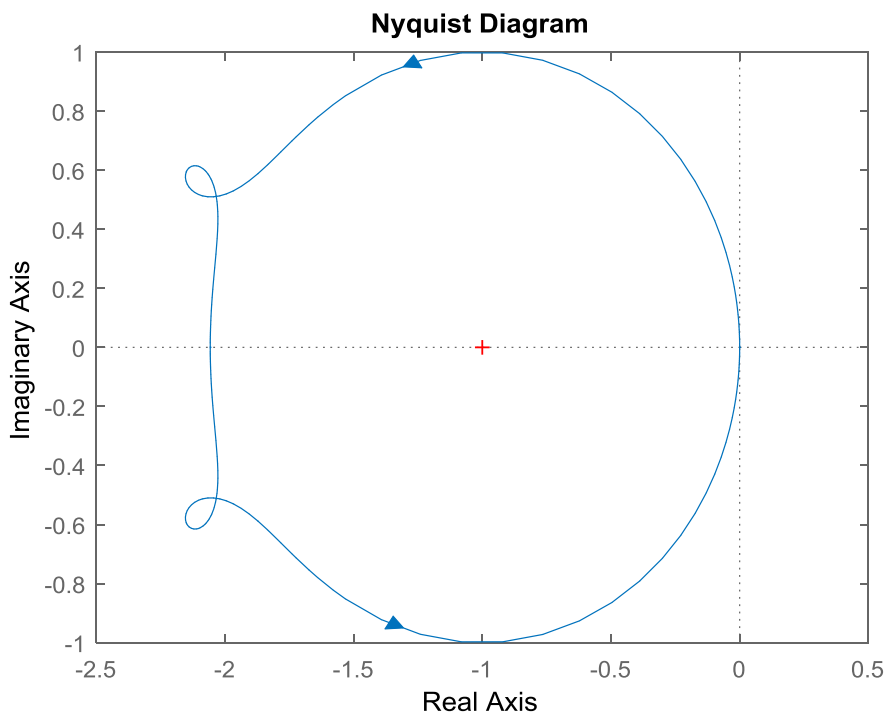
Q5.

Nyquist plot of the open-loop transfer function $L(s) = K(sI - A)^{-1}B$

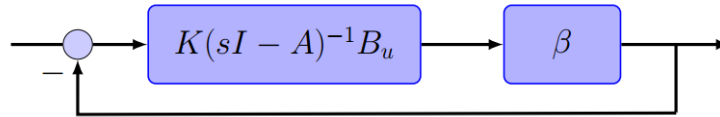
```

looptf =

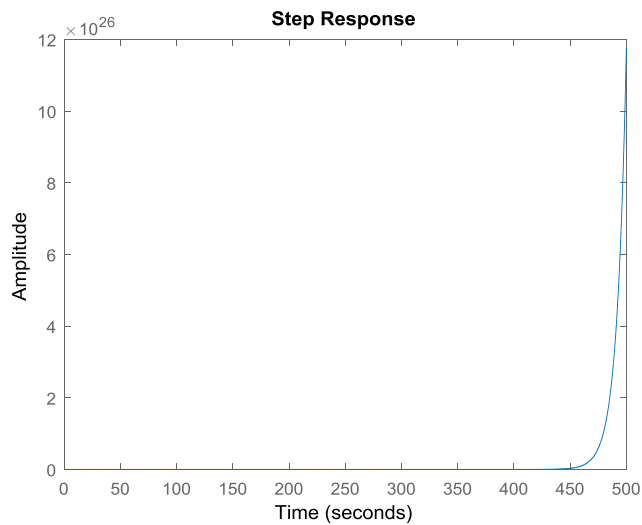
      1.486 s^3 + 2.68 s^2 + 0.3195 s + 0.1141
-----
      s^4 + 1.06 s^3 - 1.115 s^2 - 0.0658 s - 0.05547
    
```



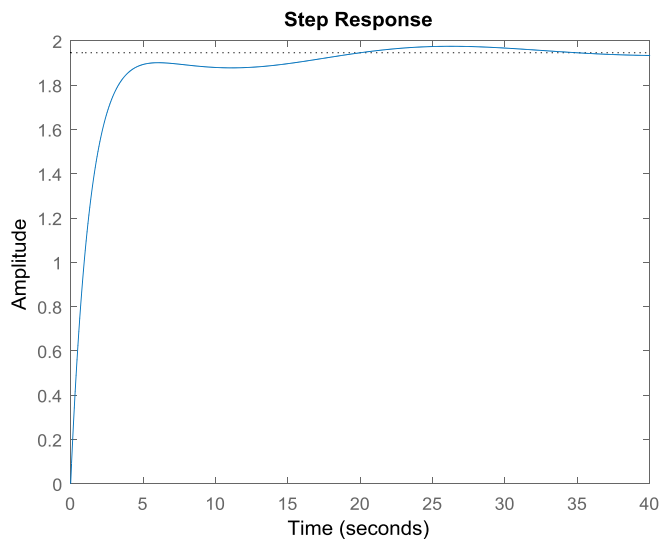
- Can study this by introducing a modification to the system, where nominally $\beta = 1$, but we would like to consider:
 - ♦ The gain $\beta \in \mathbb{R}$
 - ♦ The phase $\beta \in e^{j\phi}$



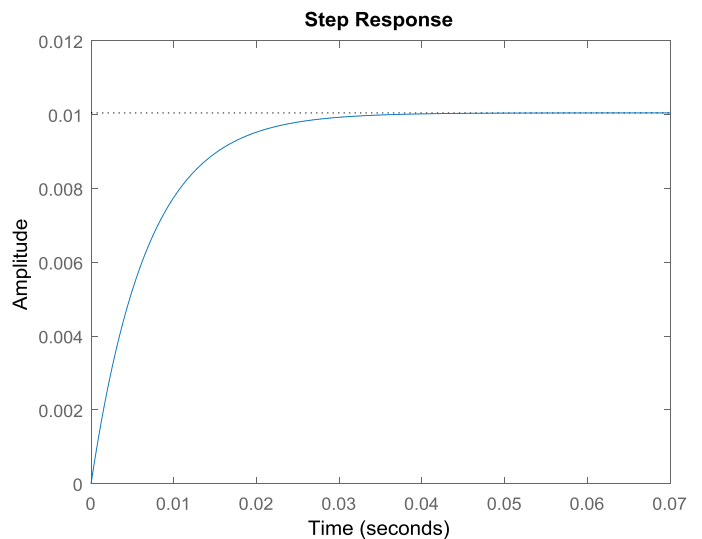
If $\beta \in (g_m, +\infty) = (0.4862, +\infty)$, the closed-loop system would be stable
 $\beta = 0.4$, unstable



$\beta = 1$, stable



$\beta = 100$, stable



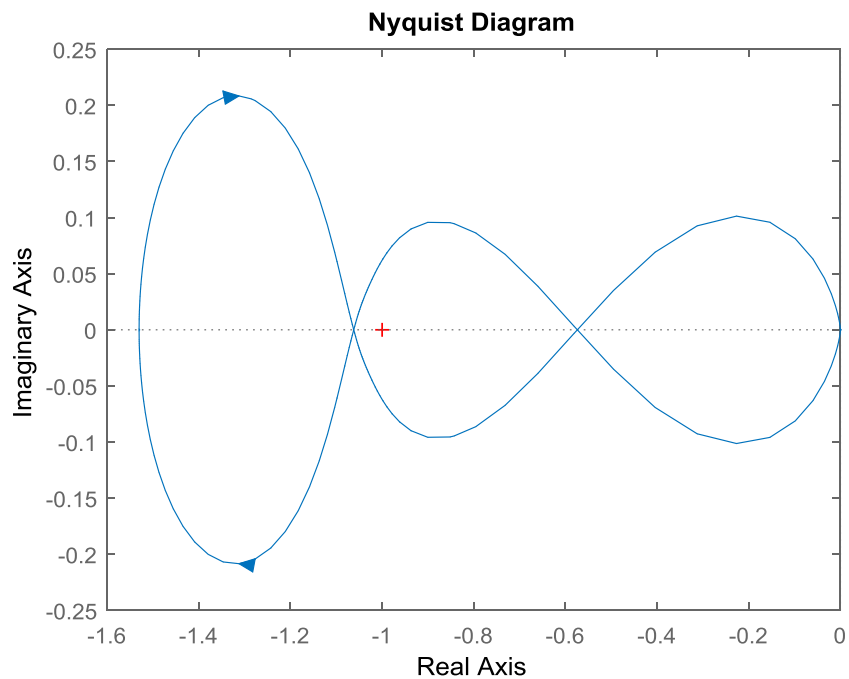
LQG transfer function from the measurement to the input

$$G_{lqg} = \frac{-14.8 s^3 - 26.51 s^2 - 2.873 s - 1.123}{s^4 + 4.028 s^3 + 6.435 s^2 + 3.735 s + 0.1158}$$

Loop transfer function of LQG design

$$\text{LoopLQG} = \frac{2.434 s^5 + 7.244 s^4 + 5.768 s^3 + 0.9765 s^2 + 0.244 s + 0.009828}{s^8 + 5.088 s^7 + 9.591 s^6 + 5.999 s^5 - 3.423 s^4 - 4.69 s^3 - 0.7318 s^2 - 0.2148 s - 0.006422}$$

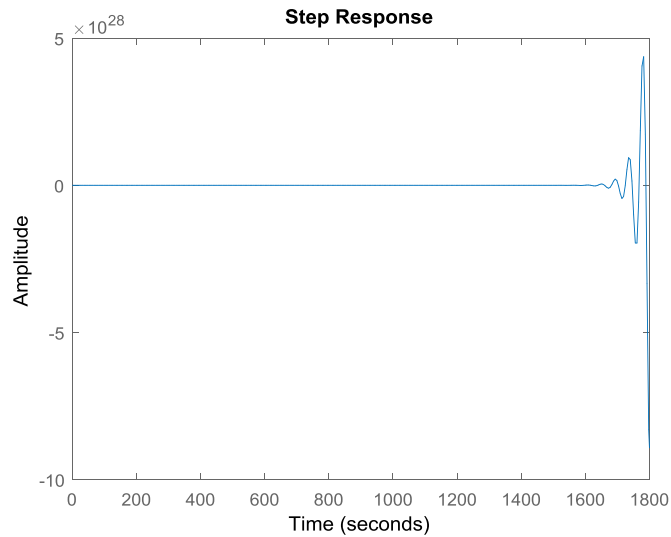
Continuous-time transfer function.



Open-loop poles (one unstable pole)

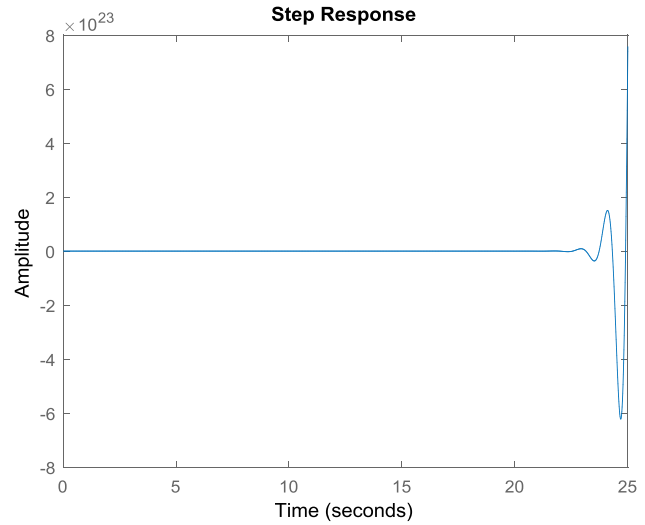
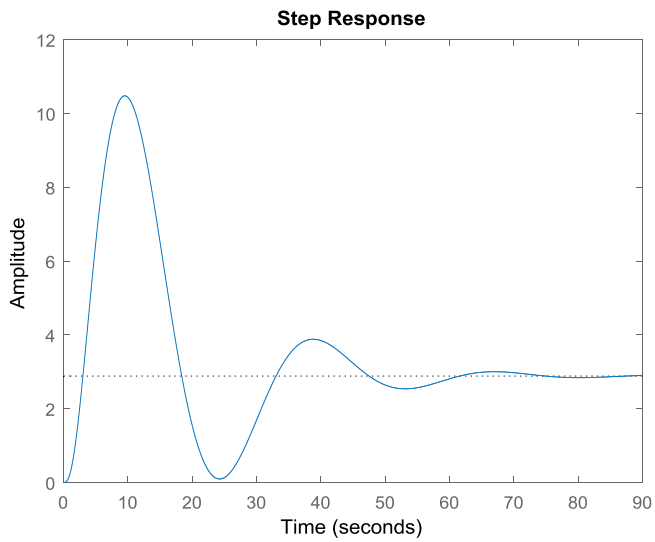
- 1.4034 + 0.9994i
- 1.4034 - 0.9994i
- 1.7036 + 0.0000i
- 1.1885 + 0.0000i
- 0.7309 + 0.0000i
- 0.0438 + 0.2065i
- 0.0438 - 0.2065i
- 0.0328 + 0.0000i

If $\beta \in (g_{m1}, g_{m2}) = (0.9417, g_{m2})$, the closed-loop system would be stable
 $\beta = 0.9$, unstable



$\beta = 1$, stable

$\beta = 100$, unstable



Q6

<code>>> Kf{2}</code>	<code>>> Kf{2}</code>	<code>>> Kf{3}</code>	<code>>> Kf{4}</code>	<code>>> Kf{5}</code>
<code>ans =</code>	<code>ans =</code>	<code>ans =</code>	<code>ans =</code>	<code>ans =</code>
-44.0222	-44.0222	-46.0067	-52.7181	-71.5250
4.9036	4.9036	11.5304	30.3977	117.8809
6.8722	6.8722	18.2762	54.3523	236.3659
3.7073	3.7073	6.0459	10.4262	21.7424

```

%% Kalman filter
F = B;
q2 = [0,10,100,1000,2e4];
Kf = cell(length(q2),1);      %% Kalman filter gain
LoopLQG = cell(length(q2),1); %% Loop transfer function of LQG controller
Gm = zeros(length(q2),1);     %% Gain margin
Pm = zeros(length(q2),1);

for i = 1:length(q2)

    W = 0.01 ; V = 1+ q2(i);

    P = are(A',C'*W^(-1)*C,F*V*F');
    Kf{i} = P*C'*W^(-1);

    %% Open-loop transfer function of LQG design
    %% L(s)=K*(sI - A + Kf*C + B*K)^(-1)*Kf*C(sI-A)^(-1)*B = sys2 * sys1 (cc
    %% sys2 = K*(sI - A + Kf*C + B*K)^(-1)*Kf;
    %% sys1 = C(sI-A)^(-1)*B

    [Num1,Den1] = ss2tf(A-Kf{i}*C-B*G,Kf{i},G,0); %% sys2
    [Num2,Den2] = ss2tf(A,B,C,0);                %% sys1

    LoopLQG{i} = series(tf(Num1,Den1),tf(Num2,Den2)); %% loop transfer fu
    [Gm(i),Pm(i),~,~] = margin(LoopLQG{i});     %% Margins
end

```

